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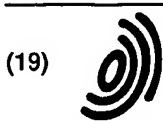
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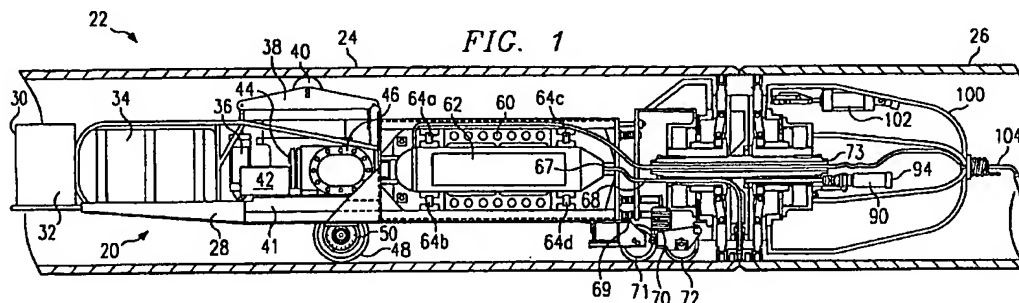
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(54) **Arc and laser welding process for pipeline**

(57) An automatic welder is used in an internal welder unit which travels along the interior of a pipeline and welds the abutting ends of the pipe segments together. The automatic welder has a carriage assembly that contains a laser source for producing a laser beam, first and second line-up clamp assemblies for aligning the respective abutting ends of the pipe segments together, at least one laser beam conductor, or alternatively a reflecting surface positioned between said first and second line-up clamp assemblies along the axis of said beam, for directing said beam to the abutting ends of said first and second pipe segments,

and a drive for rotating the reflecting surface around the axis of said beam to direct the beam to the abutting ends of said pipe segments for welding said pipe segments together. The automatic welder can also be configured as an external welder in which the automatic welder carrying a laser source is carried on a track mounted on the outside of the pipeline. As the external welder orbits around the pipeline, the laser source generates a laser beam which is directed at the junction of the abutting ends of the pipe segments for welding them together. Arc and laser beads can be combined to form a composite welding joint.



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Description

TECHNICAL FIELD OF THE INVENTION

This invention relates in general to welding and in particular to welding a pipeline using arc and laser welders together.

BACKGROUND OF THE INVENTION

Liquefied and gaseous products are typically transported over long distances most efficiently using transmission pipelines. These pipelines are generally constructed by welding together individual pipe segments at their abutting ends from the outside as well as the inside to form a continuous pipeline. The pipeline may also need internal welding on occasions where the continuity of the pipeline has been disturbed by external forces such that adjacent pipe segments are shifted relative to each other. The welding of these pipe segments has to be performed with precision and with a minimum distortion of these segments to maintain the best possible joint strength. Accordingly, an efficient, accurate and reliable welding machine is needed to perform weldings on the pipeline joints internally.

Since the joint ends of a tubular pipeline cannot be rotated about a stationary welding source, automatic pipe welding equipment typically traverses a welding mechanism circumferentially about the abutting ends of the pipe segments. Automated machines to perform this operation are shown in U.S. Pat. No. 3,612,808 to Nelson, U.S. Pat. No. 4,525,616 to Slavens, and U.S. Pat. No. 5,059,765 to Laing. However, it is desirable to have additional precision and repeatability in the welding process than those provided by the current internal welding systems employing torch or arc welding techniques. Further, conventional automated welding equipment faces a productivity trade-off: the welding machine can travel more slowly in exchange for more reliable welding or travel faster for a higher throughput, but at a higher probability of causing welding defects. The present invention aims at eliminating the above-mentioned disadvantages and accordingly provides a welding apparatus which makes it possible to obtain a uniform weld and reduce substantially the time required for welding pipe segments together to form a pipeline.

These advantages are achieved by using as a welding agent a laser beam from a movable laser source that can be positioned inside a pipeline in the vicinity of the abutting ends of the pipe segments. The advantages of using a laser beam having a power output great enough to weld together pipe segments as a welding agent include: (1) welding in single pass for faster processing, (2) welding in a room atmosphere without special environmental preparation, (3) welding more accurately, (4) welding with little or no induced contamination, (5) welding with precisely directed and concentrated energy that results in no distortion at the end of the welding, and (6)

welding with the capability of rapid starting and stopping for improved throughput.

Numerous laser welding machines have been adapted for pipeline welding. For example, U.S. Pat. No. 4,591,294, which issued on May 27, 1986 to Foulkes, discloses a pipe welding assembly in which welding of one pipe length to another is accomplished by gas lasers mounted to rotate around the axis of the pipes to weld the pipe ends together. However, the lasers disclosed in Foulkes cannot traverse the length of the pipes. U.S. Pat. No. 4,533,814, which issued on August 6, 1985 to Ward, discloses a stationary laser source whose beam is directed to the pipe joint via a flexible laser beam guide. U.S. Pat. No. 4,429,211, which issued on January 31, 1984 to Carstens et al., also discloses a laser welding system for welding 360° around a pipe. However, the laser in Carstens is mounted remotely from the welding site and requires passive and active beam alignment systems for real time compensation of angular misalignment. U.S. Pat. No. 4,080,525, which issued on March 21, 1978 to Gobetz, discloses an external welding device having laser transmitting means to orbitally direct the laser beam to the welding joints from a stationary laser source. However, a laser welding system having a laser source located remotely from the welding spot suffers from inaccuracies that result from beam misalignment, as pointed out by the laser system described in Carstens. U.S. Pat. No. 4,001,543, which issued on January 4, 1977 to Bove et al., discloses a laser positioned to direct a laser beam along the axis of the pipeline and a reflection system mounted for movement through an arc of 360° in the path of the laser beam to reflect that beam radially on the abutting ends of the pipeline.

SUMMARY OF THE INVENTION

A selected embodiment of the present invention is a method for welding abutting pipe segments at the junction of the pipe segments so that the pipe segments are joined together by a weld joint. There are two steps in this process. One of the steps comprises forming a partial weld joint at the junction of the pipe segments by operation of an arc welder which makes a circumferential pass of the pipe segments along the junction. A second of the steps is the forming of a partial weld joint at the junction by operation of a laser welder which makes a circumferential pass of the pipe segments along the junction. The two partial weld joints together, formed by the arc welder and the laser welder, form the weld joint between the pipe segments.

In a further aspect of the present invention, the arc welder is positioned internal to the pipe segments and the laser welder is positioned external to the pipe segments.

A further embodiment of the present invention comprises a method for forming a weld joint between pipe segments at a junction and includes a first step of form-

ing a root bead at the junction by operation of an internal arc welder which makes a circumferential pass of the pipe segments along the junction on the interior of the pipe segments. The method further includes the step of forming the remainder of the weld joint between the pipe segments by operation of an external laser welder which makes a circumferential pass of the pipe segments along the junction on the exterior of the pipe segments.

A further embodiment of the present invention is a method of forming a weld joint between abutting pipe segments which is produced by first forming the majority of the weld junction between the pipe segments by operation of an external laser welder which makes a circumferential pass of the pipe segments along the junction on the exterior of the pipe segments. The second step comprises forming a cap weld bead at the junction over the laser welder junction operation of an external arc welder making a circumferential pass of the pipe segments along the junction on the exterior of the pipe segments.

A still further embodiment of the present invention is a method for producing a composite weld junction for welding abutting pipe segments. The first step comprises forming a root bead of a weld joint between the pipe segments at the junction by operation of an internal arc welder which makes a circumferential pass of the pipe segments along the junction on the interior of the pipe segments. Next, there is formed an intermediate weld bead of the weld joint between the pipe segments by operation of an external laser welder which makes a circumferential pass of the pipe segments along the junction on the exterior of the pipe segments. Finally, a cap weld bead of the weld joint is formed at the junction over the intermediate weld bead by operation of an external arc welder making a circumferential pass of the pipe segments along the junction on the exterior of the pipe segments.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will now be described in more detail with reference to the accompanying drawings which illustrate the different ways of using the welding apparatus of the present invention in practice.

FIG. 1 is a longitudinal, elevational view, partly in cross-section, of a first configuration of an internal welder;

FIG. 2 is a longitudinal, cross-sectional view of the line-up clamp assembly of the internal welder of FIG. 1 during alignment;

FIG. 3 is a longitudinal, cross-sectional view of the line-up clamp assembly of the internal welder of FIG. 1 during welding;

FIG. 4 is a longitudinal, elevational view, partly in cross section, of a second configuration of an internal welder in accordance with the present invention;

FIG. 5 is a longitudinal, cross-sectional view of the line-up clamp assembly of the internal welder of FIG. 4 during alignment;

FIG. 6 is a longitudinal, cross-sectional view of the line-up clamp assembly of the internal welder of FIG. 4 during welding;

FIG. 7 is a cross-sectional view of the line-up clamp assembly of the internal welder of FIG. 4;

FIG. 8 is a longitudinal, elevational view, partly in cross section, of a third embodiment of the internal welder in accordance with the present invention;

FIG. 9 is a longitudinal, cross-sectional view of the clamp assembly of the internal welder of FIG. 8 during alignment;

FIG. 10 is a transverse cross-sectional view of the center plate of the internal welder of FIG. 8 taken along line 10-10;

FIG. 11 is a transverse cross-sectional view of an outer plate of the internal welder of FIG. 8;

FIG. 12 is an enlarged longitudinal, cross-sectional view of the mirror assembly of FIG. 8;

FIG. 13 is a longitudinal, elevational view, partially in cross section, of a fourth embodiment of an external welder;

FIG. 14 is a transverse cross-sectional view of the external welder of FIG. 14 den along line 14-14; and

FIG. 15 is a longitudinal, elevational view of a fifth configuration of an external welder;

FIG. 16 is an illustration of a laser welder which includes a wire feed which can be used in conjunction with the laser welders described herein;

FIG. 17 is a illustration of abutting, beveled pipe ends having a groove formed for welding;

FIG. 18 is a sectional illustration of abutting pipe walls with a laser weld joint;

FIG. 19 is a sectional illustration of abutting pipe walls with an arc weld root bead and a laser weld joint;

FIG. 20 is a sectional illustration of abutting pipe walls with a laser weld joint having an arc weld cap bead; and

FIG. 21 is a sectional illustration of abutting pipe walls with a laser weld joint with an arc weld root bead and an arc weld cap bead.

DETAILED DESCRIPTION

A longitudinal, elevational view of the first configuration for an internal welder unit 20 is illustrated in FIG. 1.

Referring to FIG. 1, the internal welder unit 20 is positioned within a pipeline 22. The pipeline 22 is made up of a plurality of pipe segments, including a first pipe segment 24 and a second pipe segment 26, which are joined together at their abutting ends. The internal welder unit 20 has a carriage assembly 28 for propelling and positioning the internal welder unit 20 inside the

pipeline 22. The carriage assembly 28 is essentially described in U.S. Pat. Nos. 3,612,808 to Nelson et al. which was issued on June 4, 1969, 3,632,959 to Nelson et al. which issued on Jan. 4, 1972 and 5,059,765 to Laing which issued on Oct. 22, 1991, and all three of these patents are hereby incorporated by reference.

The carriage assembly 28 has a battery compartment 30 having a battery 32 inside for supplying electricity to the internal welder unit 20. An air tank 34 is mounted on the carriage assembly 28 next to the battery compartment 30 for supplying compressed air or other suitable gas for actuation of various mechanical assemblies within internal welder unit 20, such as a pressure wheel actuator 36. Pressure wheel actuator 36 is coupled to pressure wheel mount 38 to urge a pressure wheel 40 against the interior of the pipe segment 24 for providing traction in conjunction with a drive wheel 48.

The internal welder unit 20 contains a drive wheel assembly 41 having a drive wheel motor 42 which drives a motor chain 44. Motor chain 44 drives the shaft of a gear drive unit 46, which in turn rotates the drive wheel 48 using a gear drive chain 50.

The carriage assembly 28 further contains a laser assembly 60 with a laser source 62 supported on first, second, third and fourth laser mounts 64a, 64b, 64c and 64d, respectively. The laser mounts 64a, 64b, 64c and 64d provide suspension support to laser assembly 60 to prevent unwanted shocks from damaging the laser source.

A selected laser source 62 is a ZODIAK (tm) model laser invented by Herbert J.J. Sequin. A laser source is described in U.S. Patent Nos. 4,604,752 and 5,029,173, and these patents are incorporated herein by reference. Protection for the laser assembly 60 is further afforded through a plurality of flexible mountings 69 and a vertical flexible mounting 70, which couples carriage assembly 28 to a line-up station 73. The flexible mounting 69 is provided between the forward portion of the carriage assembly 28 and the rear portion of line-up station 73 to prevent forced misalignment of any components of the internal welder unit 20 when it is clamped at the end of a pipe segment 24 or 26. The vertical flexible mounting 70 is provided between the front wheels of carriage assembly 28 and line-up station 73 to prevent unwanted shocks from damaging the laser source and to center the line-up assembly before the shoes of the line up assembly are brought into contact with the pipe.

A first front wheel 71 is attached to the front bottom portion of carriage assembly 28 to allow a second front wheel 72 to drive the carriage assembly 28 back into the pipe when the internal welder is driven too far forward. The combination of pressure wheel 40, drive wheel 48, and second front wheel 72 permit the internal welder unit 20 to be pushed or pulled within the pipeline 22 along the length of the pipeline.

During operation, the internal welding unit 20 is advanced from the weld just completed to the next junction

in the pipeline. Once the internal welder is properly positioned within the pipeline, the line-up station 73 is activated to force the abutting ends of the pipe segments 24 and 26 to be aligned and ready for laser welding. An actuator 102 provides horizontal alignment for the line-up station 73 before the engagement of the line-up station 73 with pipe segment 24.

Once the line-up station 73 is engaged with the abutting ends of pipe segments 24 and 26, a laser beam 67 is generated by the laser source 62. The laser beam 67 has a power output great enough to weld together the ends of pipe segments 24 and 26. As shown in FIG. 1, the laser beam 67, which is generated by laser source 62, passes into the line-up station 73 inside a laser beam conductor 68. The laser beam conductor 68 is preferably made up of fiber optic cables which collect the laser beam 67 coming out of the laser source 62 for transmission to the inner periphery of the abutting ends of the pipe segments 24 and 26. The laser beam conductor 68 extends essentially horizontally along the axis of the pipeline until it reaches the abutting ends of the pipe segments where it is redirected to point essentially at a 90° angle relative to the axis of the pipeline 22. The laser beam conductor 68 is then rotated around the circumference of the interior of the pipe segments 24 and 26 to deliver laser beam 67 at the pipe junction to weld the two pipe segments 24 and 26 together.

Electrical power and control signals are provided to the internal welder through signal and power cable assembly 104. The signal and power cable assembly 104 includes a set of data wires which communicate with control electronics on-board the internal welder unit 20. The signal and power cable assembly 104 also has a power cable to supplement the power coming from battery 32 during the periods where the laser source is activated. Signal and power cable assembly 104 enters the internal welder unit 20 through the tip of tubular-framed nose cone 100. The tubular-framed nose cone 100 serves to protect and support the components housed therein. The signal and power cable assembly 104 passes from the tubular-framed nose cone 100 to other components of the internal welder unit 20 through a passageway extending across a rotatable disk in line-up station 73. The internal welder unit 20 further includes a laser drive motor 90 and a position encoder 94.

The operation of the line-up station 73 and the mechanism for rotating the laser beam conductor 68 is shown in detail in FIG. 2. As shown in FIG. 2, pipe segment 24 has an inner surface 17 and outer surface 18. Within inner surface 17, the line-up station 73 includes a first double acting air cylinder assembly 126 and a second double acting air cylinder assembly 128. The air cylinder assemblies 126 and 128 actuate shoes 78a-78d to clamp the internal welder unit 20 to the pipe segments 24 and 26. There are plenty of sets of air cylinders and shoes; for example, 16 sets for each of the air cylinder assemblies. The first and second double acting

air cylinder assemblies 126 and 128 are identical in operation and the following description applies to both of the assemblies 126 and 128.

As shown on the upper left of FIG. 2, shoe 78a is attached to a shoe holder 116a. Shoe holder 116a, in turn, is attached to a cylindrical shaft 115a. The shaft 115a is connected by a link 120a to a ring 121a which is slidable along the axis of the line-up station 73. Thus, the movement of shoe 78a is restricted to only radial motion relative to the center axis of the line-up station 73. A piston 124a in the cylinder assembly 126 is attached to the remaining end of the ring 121a to apply motion of the ring 121a relative to the center axis of the line-up station 73.

Piston 124a is slidably sealed to the inner walls of a chamber 119a. Chamber 119a has an annular configuration which is coaxial with the axis of line-up station 73. When a pressurized fluid, such as compressed air or hydraulic fluid, is caused to enter chamber 119a through a port 129a, the piston 124a moves in the opposite direction toward the far end of chamber 119a to work through the intervening components and activate shoe 78a. The thus activated shoe moves radially outward to clamp against an inner surface 17 of the pipe segment 24. In a similar manner, shoe 78b moves radially outward to clamp against the inner surface of pipe segment 24. The linear motion of ring 121a engages link 120b and actuates shaft 115b to clamp shoe 78b through shoe holder 116b against the inner surface 17. Thus, to align the abutting ends of the pipe segments 24 and 26, all 16 shoes of cylinder assembly 126 are extended outward at the same time when pressurized fluid is applied to chamber 119a. When fluid pressure is admitted to the other side of chamber 119a via a second port 127a, the piston 124a moves in the opposite direction toward the first port 129a. The shoes 78a and 78b will move inward, releasing the pipe segment 24.

Once the internal welding unit is first advanced to the junction between first and second pipe segments 24 and 26, a alignment operation is carried out and then the shoes 78a and 78c are longitudinally positioned so that they can expand radially outward from the first line-up clamp assembly 74 to clamp against the inner periphery of the first pipe segment 24. The position of the first line-up clamp assembly is adjusted by the operation of the drive wheel 48 to cause the line-up station 73 to be positioned a short distance inside from the pipeline joint.

The alignment operation is assisted by the use of a plurality of aligners 101, preferably three aligners, which are equally spaced around the axis of the pipe. The aligners are raised by three corresponding actuators, such as pneumatic or hydraulic actuators 102, through parallel support arms 103a and 103b. The aligners 101 are activated and positioned facing the exposed end of pipe segment 24 before the front and rear shoes 78a-78d are raised and before the second pipe segment 26 has been butted up against the first pipe segment 24.

With the aligners 101 raised, the internal welder is backed up until the three aligners 101 are in contact with the face of the pipe segment 24. Once the internal welder unit 20 is aligned with the end of the pipe segment 24, the aligners 101 are retracted out of the way to allow the installation of the pipe segment 26 abutting pipe segment 24. Line-up station 73 also has a passageway 113 for allowing gas and electrical lines to pass from the tubular-framed nose cone 100 to the portion of the internal welder unit 20 on the other side of the line-up station 73.

The aligners 101 are then retracted out of the way and the second pipe segment is butted up against the first pipe segment. The second set of shoes 78b and 78d, and the corresponding shoes, not shown, on the second double acting air cylinder assembly 126 next extends radially outward by applying compressed air into a chamber 119b via a port 129b. Similar in operation to shoes 78a and 78c of assembly 126, a piston 124b causes a ring 121b to move toward a second port 127b. The linear motion of ring 121b drives links 120b and 120d to activate shafts 115c and 115d to clamp shoes 78c and 78d of shoe holders 116c and 116d, respectively. The radially outward extension of the second set of shoes clamps the second pipe segment 26 about the inner periphery thereof, causing the abutting ends of the pipe segments 24 and 26 to be aligned for welding. In this manner, the pipe segments 24 and 26 are aligned and ready for welding. In certain situations where the ends of the pipe segments may be disrupted such that they no longer have a precisely circular cross section, the line-up station 73 deforms the ends of the pipe segments 24 and 26 into a circular configuration at the abutting ends, as well as positioning the ends in alignment.

After the pipe segments have been buried together, the laser beam 67 is transmitted from the laser beam conductor 68 to the interior of the abutting ends of pipe segments 24 and 26 through a nozzle 83. Laser beam conductor 68 is positioned inside a rotatable disk 75. Rotatable disk 75 has a first chamber 114a and a second chamber 114b for receiving the laser beam conductor 68. In the single laser beam conductor arrangement shown in FIG. 2, laser beam conductor 68 is threaded through second chamber 114b and enters nozzle 83.

Referring also to FIG. 3, nozzle 83 has a focusing lens 79 positioned in the path of the laser beam 67 for focusing the laser beam 67 onto the abutting ends of the pipe segments 24 and 26 through the tip of nozzle 83 to a welding focus point 91. The nozzle 83 is urged against the inside of the rotatable disk 75 by compressed air provided to a nozzle chamber 85.

Rotatable disk 75 is supported by a wheel assembly 89. Each wheel 87 of a wheel assembly 89 rides along the inside surface 17 of the pipe segments. Wheel assembly 89 is attached to nozzle 83. By adjusting the position of the wheel assembly 89 with respect to the nozzle 83, the welding focus point 91 can be maintained

at the desired distance above or below the inside surface of the abutting ends of the pipe segments. The nozzle 83 also contains auxiliary gas nozzles, not shown, to disperse the metal vapor plume created during the laser welding process and shield the weld metal. Such gas shielding for welding is well known in the art.

Laser motor drive 90 rotates the rotatable disk 75 to direct the laser beam 67 exiting laser beam conductor 68 onto the abutting ends of pipe segments 24 and 26. The motor drive 90 is coupled through a shaft 95 to rotatable disk 75 through a pinion gear 96 and a ring gear 98 to rotate the nozzle 83. The movement of laser beam conductor 68 guides the laser beam 67 circumferentially around the interior of the pipeline through rotating disk 75 to weld together the abutting ends of pipe segments 24 and 26. After each revolution, the rotatable disk 75 reverses its direction for the next welding pass so as to avoid tangling the laser beam conductor 68 and damaging the laser beam conductor 68 due to over-twisting.

The laser motor drive 90 includes the position encoder 94 which produces a digital data signal indicating the position of the nozzle 83 during the laser beam. The signal from encoder 94 indicates the sweep position of the laser beam 67 around the interior of the junction of the abutting ends of pipe segments 24 and 26.

FIG. 3 illustrates the line-up station 73, as shown in FIG. 2, during welding. As shown, aligner 101 is retracted to a resting position. Laser beam 67 is guided by laser beam conductor 68 and is eventually directed through focusing lens 79 to be delivered to the welding focus point 91. Laser motor drive 90 is engaged with rotatable disk 75 to move the laser beam around the circumference of the interior 17 of the pipe segments 24 and 26.

FIG. 4 shows a second embodiment of the present invention. In this embodiment, the internal welder unit 130 is the same as internal welder unit 20 with respect to the reference numerals, except that the laser beam 67 generated by laser source 62 is split by a laser beam splitter 65 into four laser beams that are carried by laser beam conductors. Laser beams 266a and 266b are illustrated in FIG. 5. The longitudinal, elevational view of FIG. 4 shows only two laser beam conductors 268a and 268b, while the remaining laser beam conductors 268c and 268d and their associated components are shown in FIG. 7. These laser beam conductors enter a line-up station 143 to be redirected to aim circumferentially toward the interior surface of pipeline 22.

FIG. 5 is an enlarged longitudinal, cross-sectional, partial view of the embodiment of FIG. 4 which illustrates the alignment of the laser beams with the abutting end of first pipe segment 24. As shown in FIG. 5, line-up station 143 has a first double acting air cylinder assembly 226 and a second double acting air cylinder assembly 228 that are operationally identical to the cylinder assemblies 126 and 128 described in reference to FIG. 2.

Line-up station 143 contains a total of four laser beam conductors 268a-268d, although only laser beam conductors 268a and 268b are shown in FIG. 5. As shown in FIG. 5, laser beam conductors 268a and 268b are threaded through chambers 214a and 214b in a rotatable disk 275 and enters nozzles 283a and 283b having focusing lens 279a and 279b. Nozzles 283a and 283b are urged against the inside of rotatable disk 275 by compressed air provided to nozzle chambers 285a-285d. See note FIG. 5. Each of nozzles 283a and 283b is functionally identical to nozzle 83 of FIG. 2. The laser beams 266a and 266b are focused onto the abutting ends of the pipe segments 24 and 26 through the tip of nozzles 283a and 283b to welding focus points 291a and 291b. Although FIG. 5 shows only two laser beam conductors, the description of laser beam conductors 268a and 268b is equally applicable to laser beam conductors 268c and 268d which are shown in FIG. 1.

During alignment, the line-up station 143 is moved slightly beyond the end of pipe segment 24. Aligners 101 are activated and the line-up station 143 is adjusted to align the focusing lens 279a and 279b with the end of pipe segment 24 as described in reference to FIG. 2.

FIG. 6 illustrates the welding operation of the four laser beam system shown in FIG. 5. In FIG. 6, the aligners 102 are retracted and the second pipe segment 26 has then positioned against the first pipe segment 24. A second set of shoes on the second double acting all cylinder assembly 228 expands radially outward to clamp the second pipe segment 26. Next, the laser beam 67 is transmitted from laser source 62 to beam splitter 65, which splits the laser beam into four laser beams 266a-266d, only two of which are shown in the longitudinal, cross-sectional view of FIG. 6. The two laser beams 266a and 266b are transmitted through laser beam conductors 268a and 268b to the interior of the abutting ends of pipe segments 24 and 26 through nozzles 283a and 283b. It is understood that the foregoing description of laser beam conductors 268a-268b are also applicable to the hidden laser beam conductors 268c-268d of FIG. 6. Because the delivery of the laser beam is accomplished via four laser beam conductors, the line-up station 143 only needs to rotate the disk 275 by 90° to provide complete coverage of the interior circumference of the junction of pipe segments 24 and 26. After each quarter revolution, the rotatable disk 275 reverses its direction for the next welding pass so as to avoid tangling or stressing the laser beam conductors 268a-268d.

While FIG. 6 shows only two of the four laser beam conductors, FIG. 7 illustrates the placement of the four laser beam conductors 268a, 268b, 268c and 268d. In FIG. 7, each shoe holder 216 has shoes 278a and 278c. During operation, all 16 shoe holders, including the wheel assemblies carrying the nozzles 283a-283d, extend radially outward to clamp the inner circumference of the pipe segments 24 and 26. The laser beams are focused by lens 279a, 279b, 279c and 279d. The

beams exit through nozzles 283a, 283b, 283c, and 283d to direct the laser beams to focus points 291a, 291b, 291c and 291d to weld together the ends of the pipe segments. Under this arrangement, the line-up station 143 only needs to rotate disk 275 by 90° to provide complete coverage of the circumference of the pipe segments 24 and 26.

FIG. 8 shows a third welder configuration. In this embodiment, the internal welder unit 150 is the same as internal welder unit 20 with respect to the reference numerals, except the laser beam conductor 68 of line-up station 152 is replaced with a reflecting surface 365. The reflecting surface 365, preferably a mirror, reflects the laser beam 67 coming out of the laser source 62 for transmission to the inner periphery of the abutting ends of the pipe segments 24 and 26. The reflecting surface 365 is mounted inside rotatable disk 353 for reflecting and directing laser beam 67 essentially at a 90° angle relative to the axis of the pipeline 22 at the abutting ends of pipe segments 24 and 26. Rotatable disk 353 is driven by laser motor drive 390 whose rotations are monitored by position encoder 394.

FIG. 9 is a enlarged longitudinal, cross-sectional view of a portion of the embodiment of FIG. 8 showing the alignment of line-up station 152 with pipe segment 24. The line-up station 152 arrangement is similar to that of FIG. 2, except that line-up station 152 has been modified for the substitution of a reflecting surface 365 in place of laser conductor 68.

The line-up station 152 consists of a first double acting air cylinder assembly 326 and a second double acting air cylinder assembly 328. Each of the double acting air cylinder assemblies 326 and 328 is identical in operation to the double acting air cylinder assemblies 126 and 128 described in reference to FIG. 2.

The alignment operation of line-up station 152 is similar to that of line-up station 73 of FIG. 2. After the pipe segments have been aligned, the aligners 101 are retracted and the second set of shoes on the second double acting air cylinder assembly 328 expands radially outward and clamps against the inner periphery of the second pipe segment 26. Next, the laser beam 67 is transmitted from laser source 62 to the reflecting surface 365, which redirects the laser beam 67 to the interior 17 of the abutting ends of pipe segments 24 and 26 through nozzle 385.

Reflecting surface 365 is positioned inside a rotatable disk 380, further shown in FIG. 11. Rotatable disk, or center plate, 380 is sandwiched between two outer plates 388a and 388b, which are further shown in FIGS. 11 and 12. Rotatable disk 380 includes a nozzle 385 for delivering the laser beam 67 to the inner circumference of pipe segments 24 and 26. Nozzle 385 has a focusing lens 379 positioned in the path of the laser beam 67 for focusing the laser beam 67 onto the abutting ends of the pipe segments 24 and 26 through the tip of nozzle 385 to a welding focus point 391.

A laser motor drive 390 rotates the rotatable disk

375 to direct the laser beam 67 exiting the reflecting surface 365 onto the abutting ends of pipe segments 24 and 26. The shaft of motorized drive 390 is coupled with rotatable disk 375 through pinion gear 396 and ring gear 398 to rotate disk 375. As shown in FIG. 9, the movement of reflecting surface 365 guides the laser beam 67 circumferentially around the interior of the pipeline through rotating disk 375 to weld together the abutting ends of pipe segments 24 and 26.

FIG. 10 is a cross-sectional view of the rotatable disk, or center plate, 380 for the internal welder shown in FIG. 10. The reflecting surface 365 is housed in space 391 for directing the laser beam through focusing lens 379 to the welding focus point 391. The rotatable disk, or center plate, 380 includes four gear bearing holes 384a-384d containing hollow gears 386a-386d. The hollow gears 386a-386d enable gas lines and electrical trunks to be passed through the line-up station 152. Center plate 380 also has seven bearing holes 382a-382g equally spaced out on the periphery of center plate 380. Members 383a-383g penetrate through bearing holes 382a-382g to clamp first outer plate 388a, center plate 380 and second outer plate 388b together. As shown in FIG. 10, bearing holes 382a-382g are equally spaced at every two recesses 392 that house the roller shafts for the shoes.

FIG. 11 is a cross-sectional view of the outer plate 388a for the internal welder of FIG. 9. Because outer plate 388a is representative of outer plate 388b, the description of outer plate 388a also applies to that of outer plate 388b.

Outer plate 388a contains a plurality of recesses 392 housing roller shafts. The outer plate 388a further has a plurality of gears 394a-394d for a plurality of hollow gears 386a-386d. The gears 394a-394d are in contact with gear teeth 387 to receive the rotational energy to drive the rotatable disk, or center plate, 380. Further, gears 394a-394d are hollow, allowing gas lines and electrical trunks to pass through the plates and supply the other side of the internal welder unit.

A more detailed cross-sectional view of the combination of outer plate 388a, center plate 380 and outer plate 388b is shown in FIG. 12. Members 383a and 383d protrude through bearing holes 382a and 382d to clamp first outer plate 388a, center plate 380 and second outer plate 388b together. Hollow tubes 386a and 386c inside gears 394a and 394c enable gas lines and electric trunks to traverse through plates 388a, 380 and 388b to get to the other side of the internal welder unit. As shown in FIG. 12, reflecting surface frames 335a and 335b provides structural support for mounting the reflecting surface, not shown, in the center plate 380. Further, ring gear 398 is in contact with center plate 380 to deliver rotational energy generated by laser motor drive 390 to center plate 380.

FIG. 13 shows a longitudinal view of a fourth configuration where the welder carriage assembly is mounted externally on a pipeline. Externally mounted welders are

disclosed in U.S. Pat. Nos. 3,718,798 to Randolph et al. which issued on Feb. 27, 1973 and 3,806,694 to Nelson et al. which issued on Apr. 23, 1974. These two patents are incorporated herein by reference. Representative welders that have a drive assembly for positioning the welder along the gap at the junction of the abutting ends of the pipe segments are shown in U.S. Pat. Nos. 3,193,656 to Bell et al. which issued on July 6, 1965, 3,974,356 to Nelson et al. which issued on Aug. 10, 1976, 4,151,395 to Kushner et al. which issued on Apr. 24, 1979. These three patents are incorporated herein by reference.

In FIG. 13, the pipeline 432 is made up of a plurality of pipe segments, including a first pipe segment 434 and a second pipe segment 436, which are joined together at their abutting ends. In this embodiment, first and second tracks 440 and 442 are mounted on the outside circumference of the pipe segment 434. The external welder unit 438 is attached to the pipe segment 434 via first and second tracks 440 and 442, which carry the external welder unit 438 orbitally around the axis of pipeline 432. The external welder unit 438 includes a carriage assembly 439 containing the laser source 462 and drive assembly 456 for propelling the external welder unit 438 orbitally around the outside of the pipeline 432.

The external welder unit 438 is coupled to first and second tracks 440 and 442 through first and second mounting legs 448 and 450. The carriage assembly 439 of the external welder unit 438 is attached to the first and second mounting legs through carriage mount 452. The first mounting leg 448 has a first gear coupling box 444 and the second leg 450 has a second gear coupling box 446. An axle 445 mechanically links the first and second gear coupling boxes 444 and 446 so that the drive assembly 456 is mechanically coupled to both first and second gear coupling boxes 444 and 446. Each of the first and second gear coupling boxes 444 and 446 has a set of front gear wheel 447 and rear gear wheels 449 that engage with the slots on the tracks 440 and 442 to provide for the rotation of the external welder unit 438. In this manner, drive assembly 456 is mechanically linked with the front and rear gear wheels 447 and 449 of the first and second mounting legs 448 and 450 to permit the external welder unit 438 to be rotated orbitally around the axis of pipeline 432 upon activation of the drive assembly 456.

The carriage assembly 439 of the external welder unit 438 contains a laser source 462 supported on a flexible mountings 454. Flexible mountings 454 are provided between the mounting legs 448 and 450 and the base of the laser source 462 to prevent unwanted shocks from damaging the laser source. The laser source 462 generates a laser beam 467 which is directed essentially along the orbital axis of the external welder 438. The laser beam 467 has a power output great enough to weld together pipe segments 434 and 436. A hood assembly 463 shields the laser beam 467

from the point it exits laser source 462 to the point where the laser beam 467 enters the reflecting surface assembly 479. The hood assembly 463 is mounted to external welder unit 438 by hood frame 466. Nozzle 483 is mechanically supported by nozzle frame 465 and attached to the external welder through nozzle coupling 464. A handle 458 is provided on top of the external welder unit to facilitate movement of the external welder unit.

During operation, the external welding unit is advanced from the weld just completed to the next end of the pipeline. Once the external welder is properly mounted on the pipeline, the laser source is turned on to generate the laser beam. The reflecting surface assembly 479 deflects the laser beam 467 through the tip of nozzle 483 to the external junction of the pipeline to weld together the abutting ends of pipe segments 24 and 26. The drive assembly 456 is then engaged to rotate the external welder unit 438 so as to direct the laser beam circumferentially along the junction of abutting ends of pipe segments 434 and 436 to weld them together.

FIG. 14 is a cross-sectional view of the external welder carriage for use in conjunction with the fourth configuration shown in FIG. 13. In FIG. 14, tracks 440 and 442 are mounted on pipe segment 434. Tracks 440 and 442 carry the external welder 438 so as to permit external welder 438 to orbitally rotate around the center of the pipeline 432. FIG. 14 shows the front and rear gear wheels 447 and 449 engaging with tracks 440 and 442 to permit movement by the external welder 438. FIG. 12 also shows fins 490, 492 and 494 projecting from the carriage assembly 439 of the external welder unit to facilitate movement of the external welder unit 438.

The internal welder unit 20 can be functionally coordinated with the external welder unit 438 to have the external welder working into the heat generated by the internal welder. This coordination can provide for an improved joint and can enhance the speed of operation for the overall welding procedure.

FIG. 15 is a longitudinal view of a fifth configuration where the welder carriage assembly is mounted externally on a pipeline. In FIG. 15, the external welder unit 539 is attached to pipe segments 434 and 436, which are joined together at their abutting ends. Pipes 434 and 436 are further clamped by first and second tracks 440 and 442. As shown in FIG. 15, the external welder unit 539 includes a laser source 462 with mount brackets 510 and 520 extending laterally from laser source 46. The laser source 462 generates a laser beam whose output is focused by an adjustable focusing lens 564.

The welder unit 539 is coupled to the first and second gear coupling boxes 444 and 446 via a first and second legs 558 and 559. In the operating manner disclosed in FIG. 14, the drive assembly 456 is mechanically linked via axle 445 with the wheels located in the bottom of the first and second legs 558 and 559 to per-

mit the external welder unit 539 to rotate orbitally around the axis of pipeline 432 upon engagement of the drive assembly 456. Upon activation, laser source 462 delivers a laser beam circumferentially on the outside of the abutting ends of pipe segments 434 and 436 and weld the segments together.

A laser welder, such as described herein, may include a wire feed for assisting the formation of the weld junction. Referring to Fig. 16, there is shown a laser welder 600 for producing a weld joint between a pipe segment 602 having chamfered surfaces 604 and 605 and a similar pipe segment. The abutting ends of the pipe segment 602 and the similar pipe segment, not shown, are both beveled to form circumferential grooves 606 and 607. The welder 600 produces a focused laser beam 608 which is concentrated at the abutting ends of the pipe segments. The laser beam 608 is directed through a conical metal shield 610 which prevents ambient gas, smoke, spatter metal and other materials from interfering with the laser beam. A feed wire 612 is supplied from a reel, not shown, and is directed through a guide 614 so that the tip of the wire 612 is fed into the groove 606.

A bracket 620 is connected to the shield 610 for supporting gas lines 622 and 624. The gas line 622 is supplied with an inert gas such as argon which floods the welding zone to exclude oxygen and thereby prevent unwanted oxidation. The gas line 624 is supplied with an inert gas such as helium which is blown across the welding one to remove the plasma plume produced by the laser beam 608 so that the plume does not block the laser beam and prevent it from being directed to the welding joint.

An internal pipeline arc welder which can produce a welding bead while operating on the interior of abutting pipe segments is shown in U.S. Patent Nos. 3,612,808, 3,632,959 and 5,059,765, which are incorporated herein by reference. A gas metal arc welder for producing an arc weld bead on the exterior of abutted pipe segments is shown in U.S. Patent Nos. 3,718,798 and 3,806,694, which are also incorporated herein by reference. The combination use of internal and external gas metal arc welders, together with an external laser welder, as described herein, produces weld joints as shown in Figs. 19, 20 and 21.

The make-up of pipe end segments for welding is illustrated in Fig. 17. The walls of pipe segments 650 and 652 are machined to form grooves 653 and 654 when the pipe segments are abutted. Each wall of the pipe segments is chamfered to have an angle of approximately 37.5 degrees from the vertical, as-shown. The preferable depth of the groove is approximately .060 inch. The wall thickness of the pipe segments can vary as desired for the pipe used and can range, for example, from .3 inch to 1.25 inch.

Figs. 17-21 show only wall portions of pipe segments, not an entire pipe.

Referring to Fig. 18, there are shown pipe seg-

ments 660 and 662 which have been welded together by producing a weld junction 664. The weld junction 664 is produced by use of an external laser welder making a circumferential pass around the exterior of the pipe segments 660 and 662. Such an external laser welder is shown above in Figures 13, 14 and 15.

A composite weld junction is shown in Fig. 19 for pipe segments 670 and 672. A root weld bead 674 is preferably produced by an internal gas metal arc welder making a circumferential pass within the interior of the pipe segments 670 and 672. Such an internal arc welder is shown in U.S. Patent No.3,612,808. A remainder weld bead 676 which completes the weld joint between pipe segments 670 and 672 is produced by an external laser welder as described above and as shown in Figures 13-15.

A further composite weld joint is shown in Fig. 20. The weld joint between pipe segments 680 and 682 comprises a laser weld joint 684 produced by an external laser welder as described above in Figs. 13-15. A cap weld bead 686 is produced on the top of the laser weld bead 684 by operation of an external arc welder, such as shown in U. S. Patent No.3,718,798. The combination of the weld beads 684 and 686 produces the composite weld joint between the pipe segments 680 and 682.

A still further composite weld joint in accordance with the present invention is shown in Fig. 21 for pipe segments 690 and 692. The weld joint between the pipe segments 690 and 692 is formed in three stages. A root bead 694 is produced by an internal arc welder, such as referred to in the description for Fig. 19 above. The internal arc welder makes an interior circumferential pass along the junction between the pipe segments 690 and 692 to produce the weld bead 694. An intermediate weld bead 696 is produced by an external laser welder, as described above, which traverses circumferentially around the exterior of the pipe segments 690 and 692. A cap bead 698 is formed on the top of the intermediate bead 696 by operation of an external arc welder, such as described in reference to Fig. 20. The composite weld joint between the pipe segments 690 and 692 comprises the group of weld beads 694, 696 and 698.

Although several embodiments of the invention have been illustrated in the accompanying description and the drawings, it will be understood that the invention is not limited to the embodiments disclosed, but is capable of a variety of modifications and substitutions without departing from the scope of the invention.

Claims

1. A method for welding abutting pipe segments at the junction of the pipe segments, comprising the steps of:

forming a partial weld joint at said junction by operation of an arc welder making a circumfer-

ential pass of said pipe segments along said junction,

forming a partial weld joint at said junction by operation of a laser welder making a circumferential pass of said pipe segments along said junction, and

wherein said arc welder partial weld joint and said laser welder partial weld joint together form a weld joint between said pipe segments.

2. A method for welding abutting pipe segments as recited in Claim 1 wherein said arc welder is internal to said pipe segments and said laser welder is external to said pipe segments.

3. A method for welding abutting pipe segments as recited in Claim 1 wherein said laser welder uses a wire feed in forming the corresponding partial weld joint.

4. A method for welding abutting pipe segments at the junction of the pipe segments, comprising the steps of:

forming a root bead at said junction by operation of an internal arc welder making a circumferential pass of said pipe segments along said junction on the interior of said pipe segments, and
forming the remainder of a weld junction between said pipe segments by operation of an external laser welder making a circumferential pass of said pipe segments along said junction on the exterior of said pipe segments.

5. A method for welding abutting pipe segments as recited in Claim 4 wherein said laser welder uses a wire feed in forming said remainder of said weld junction.

6. A method for welding abutting pipe segments at the junction of the pipe segments, comprising the steps of:

forming the majority of a weld junction between said pipe segments by operation of an external laser welder making a circumferential pass of said pipe segments along said junction on the exterior of said pipe segments, and
forming a cap weld bead at said junction over said laser welder junction by operation of an external arc welder making a circumferential pass of said pipe segments along said junction on the exterior of said pipe segments.

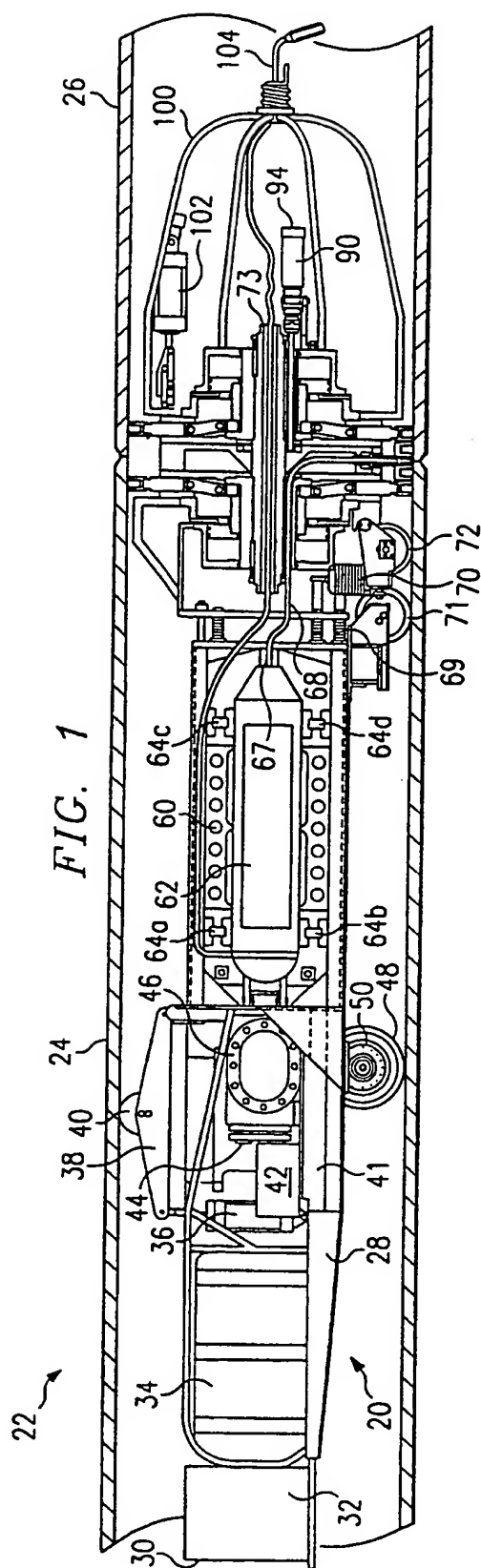
7. A method for welding abutting pipe segments as recited in Claim 6 wherein said laser welder uses a

wire feed in forming said majority of a weld junction.

8. A method for welding abutting pipe segments at the junction of the pipe segments, comprising the steps of:

forming a root bead of a weld joint between said pipe segments at said junction by operation of an internal arc welder making a circumferential pass of said pipe segments along said junction on the interior of said pipe segments, forming an intermediate weld bead of said weld joint between said pipe segments by operation of an external laser welder making a circumferential pass of said pipe segments along said junction on the exterior of said pipe segments, and
forming a cap weld bead of said weld joint at said junction over said intermediate weld bead by operation of an external arc welder making a circumferential pass of said pipe segments along said junction on the exterior of said pipe segments.

9. A method for welding abutting pipe segments as recited in Claim 8 wherein said laser welder uses a wire feed in forming said intermediate weld bead of said weld junction.



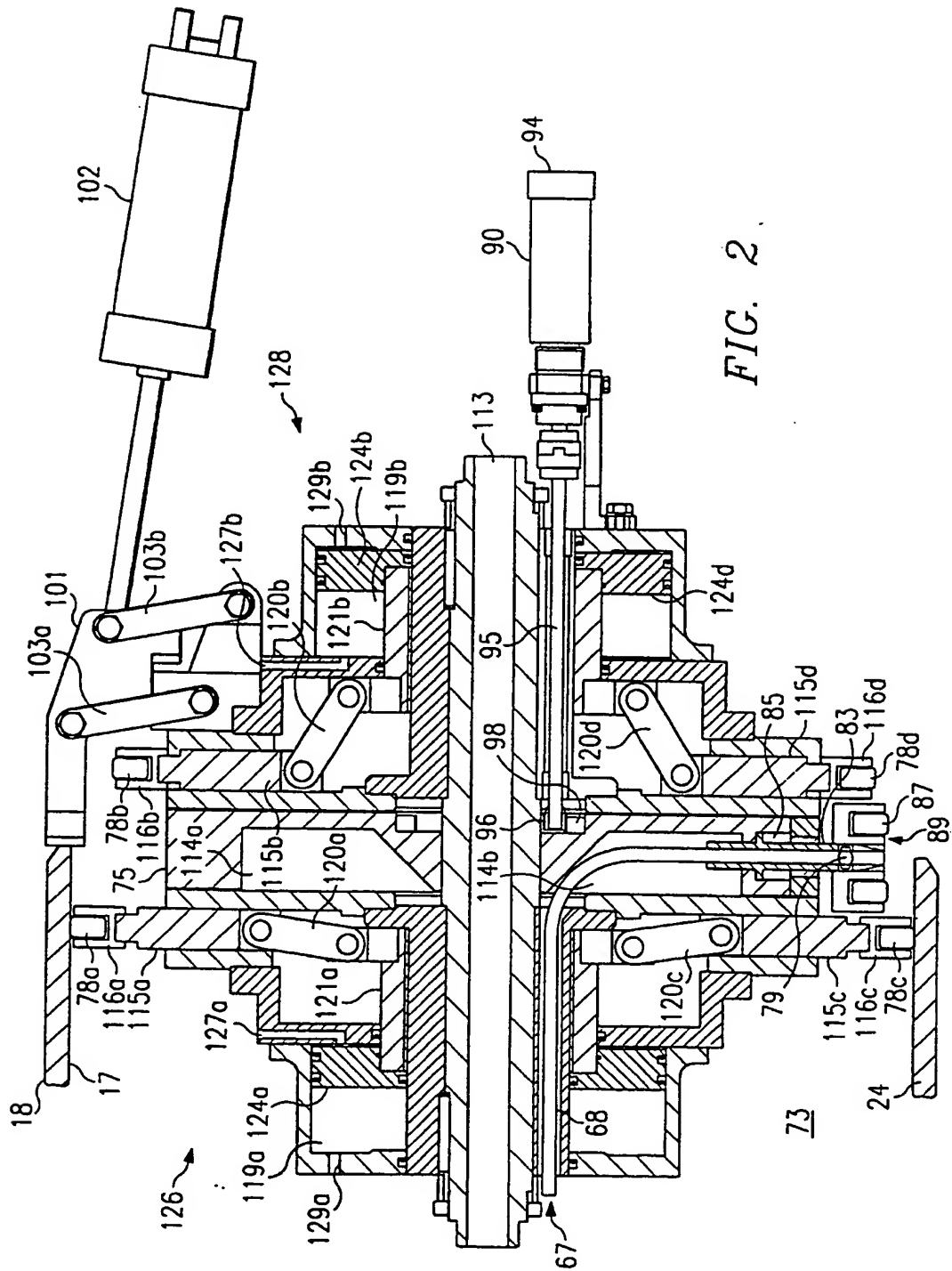


FIG. 2

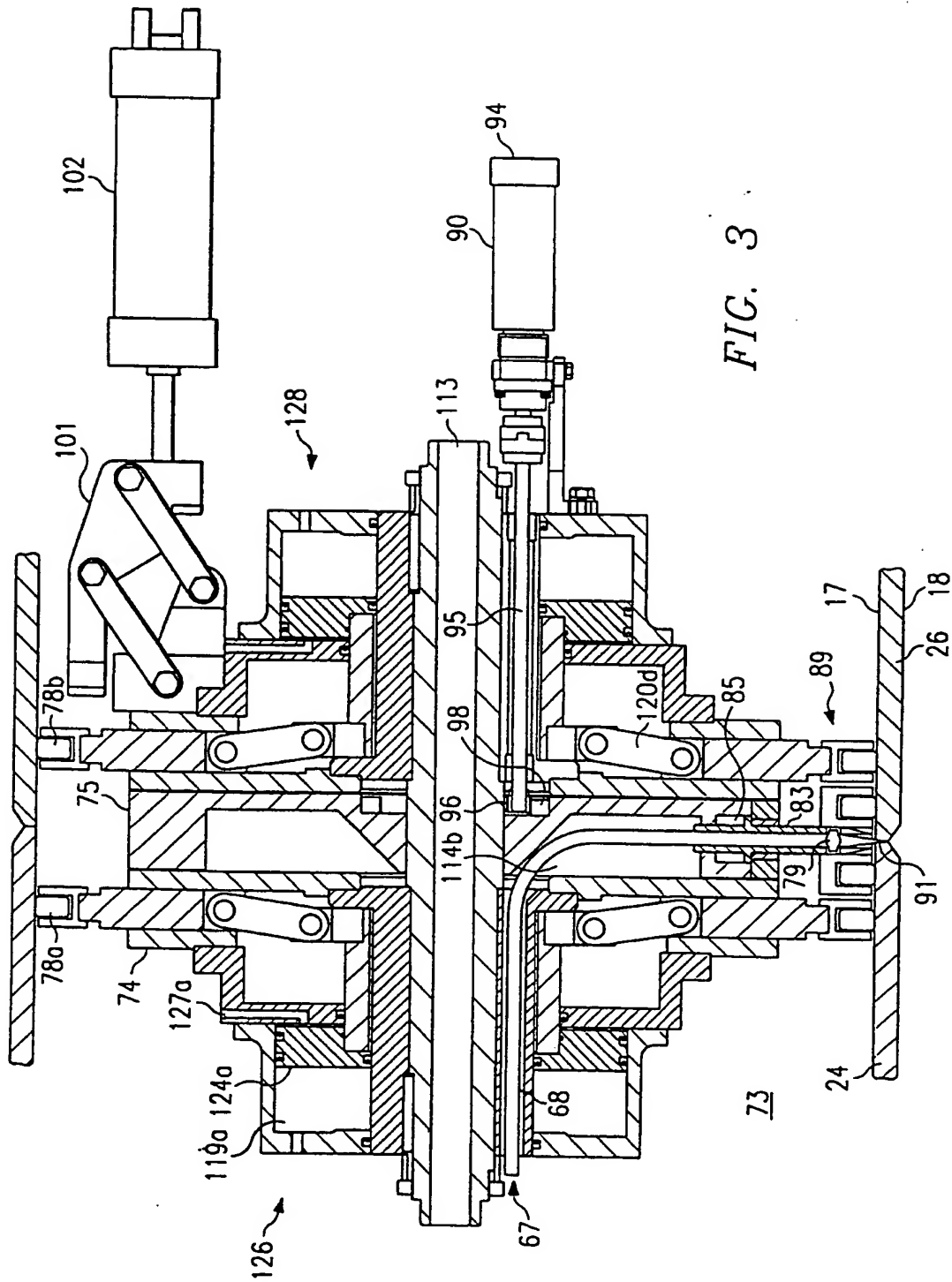
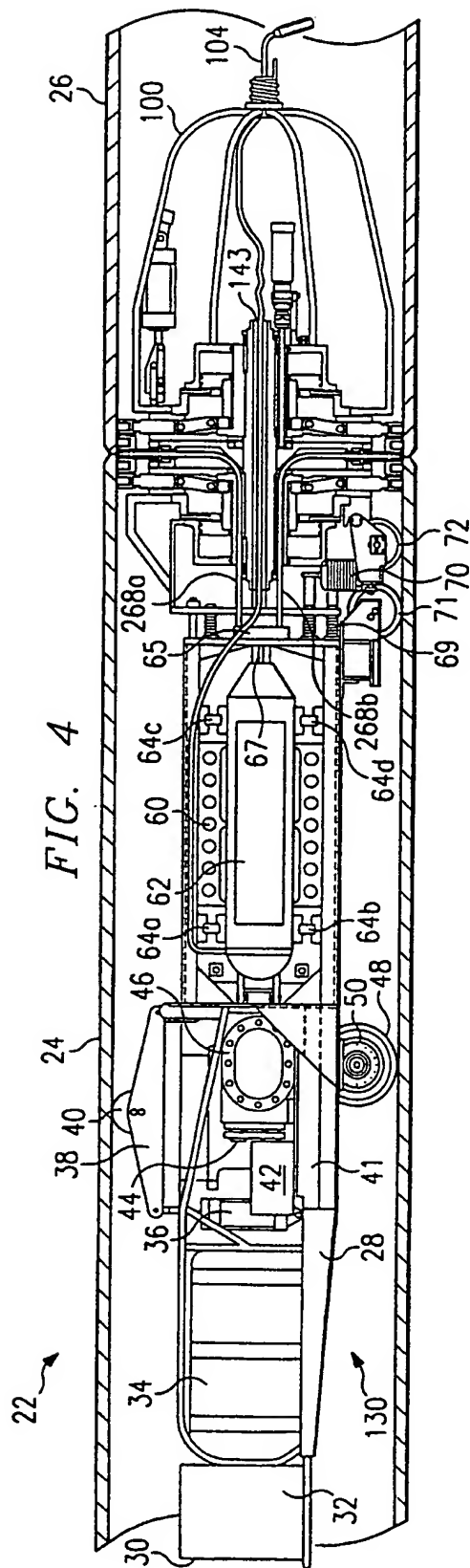
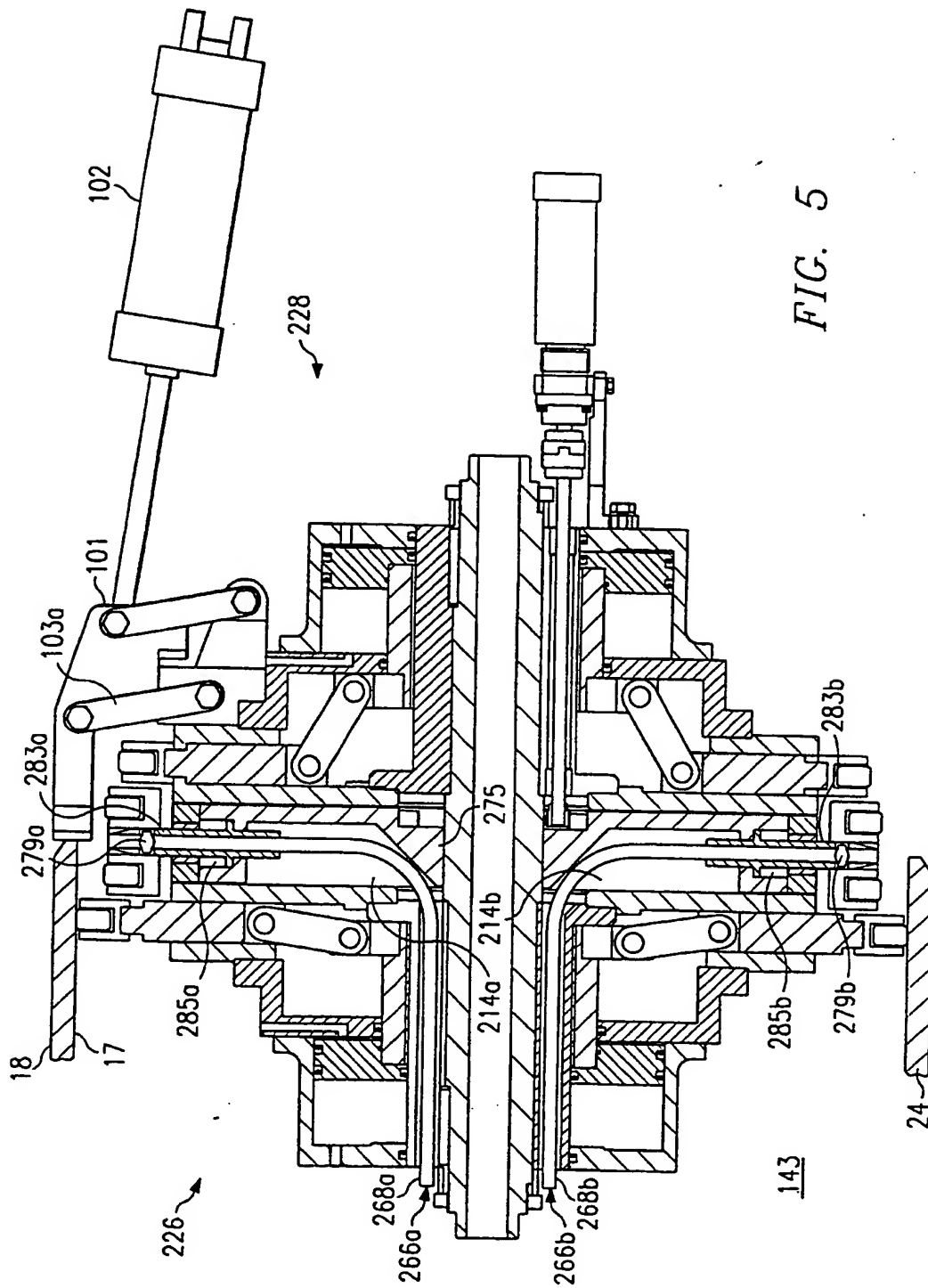
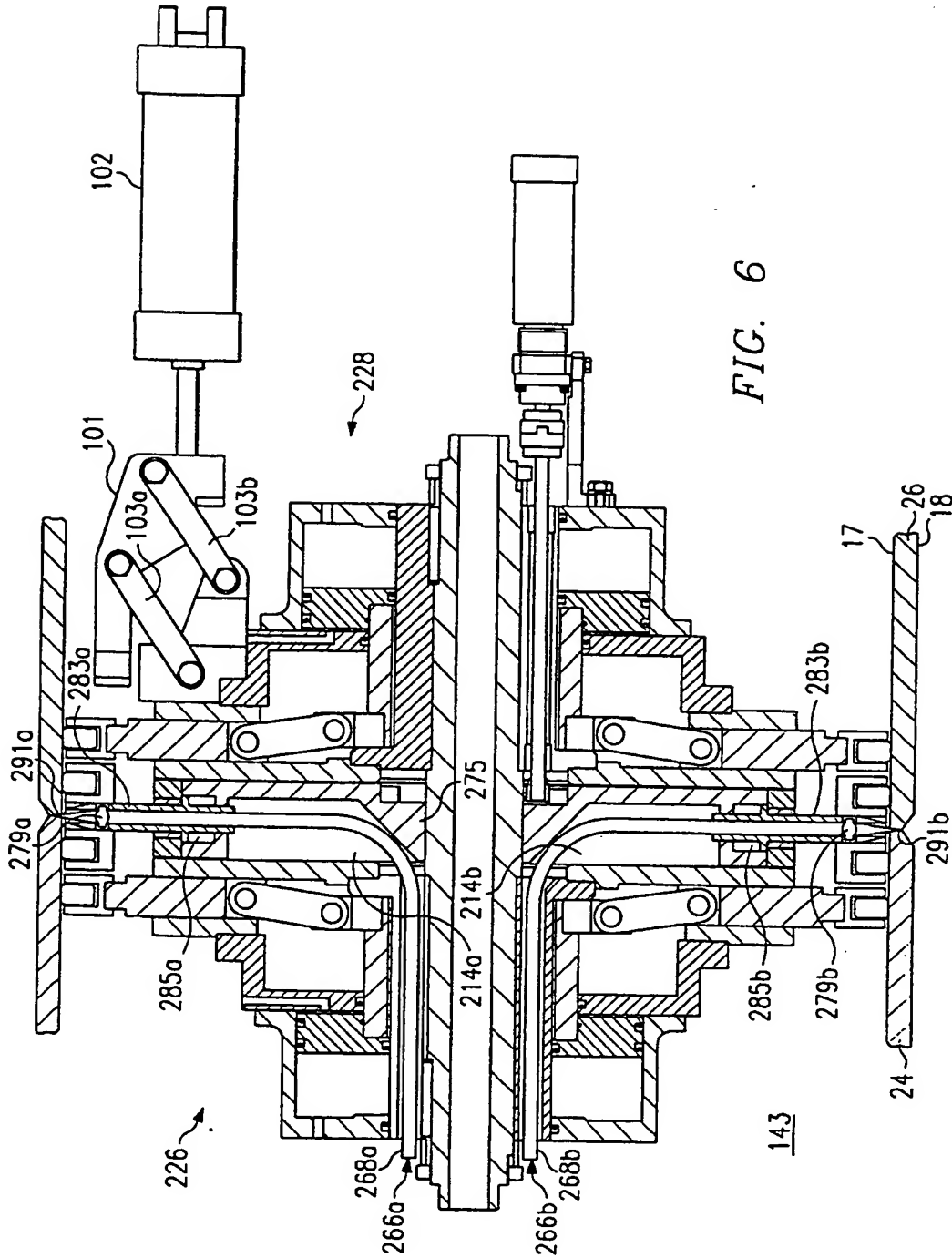


FIG. 3







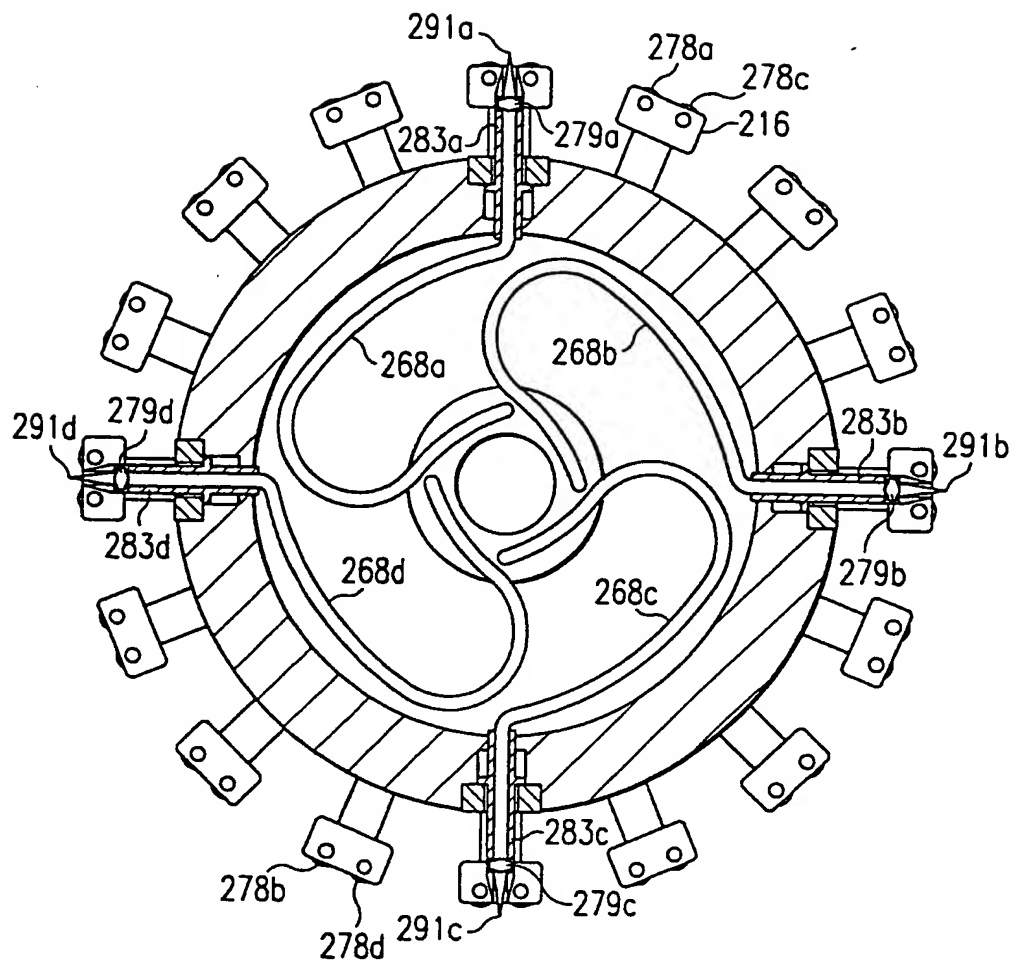
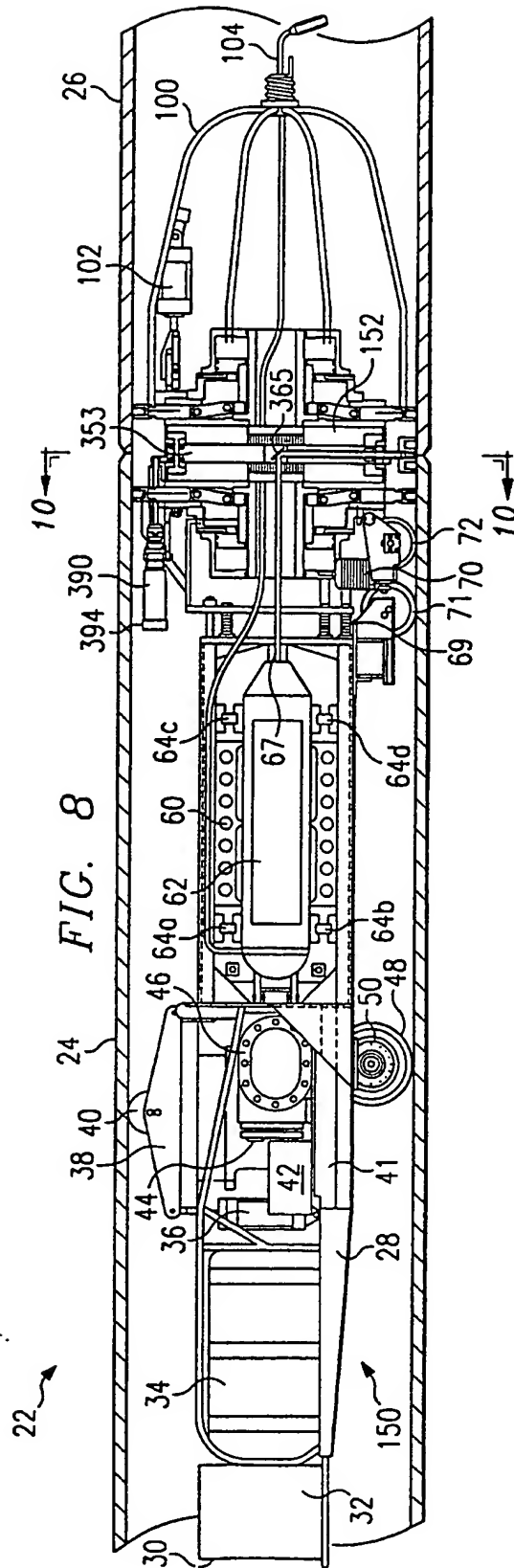


FIG. 7



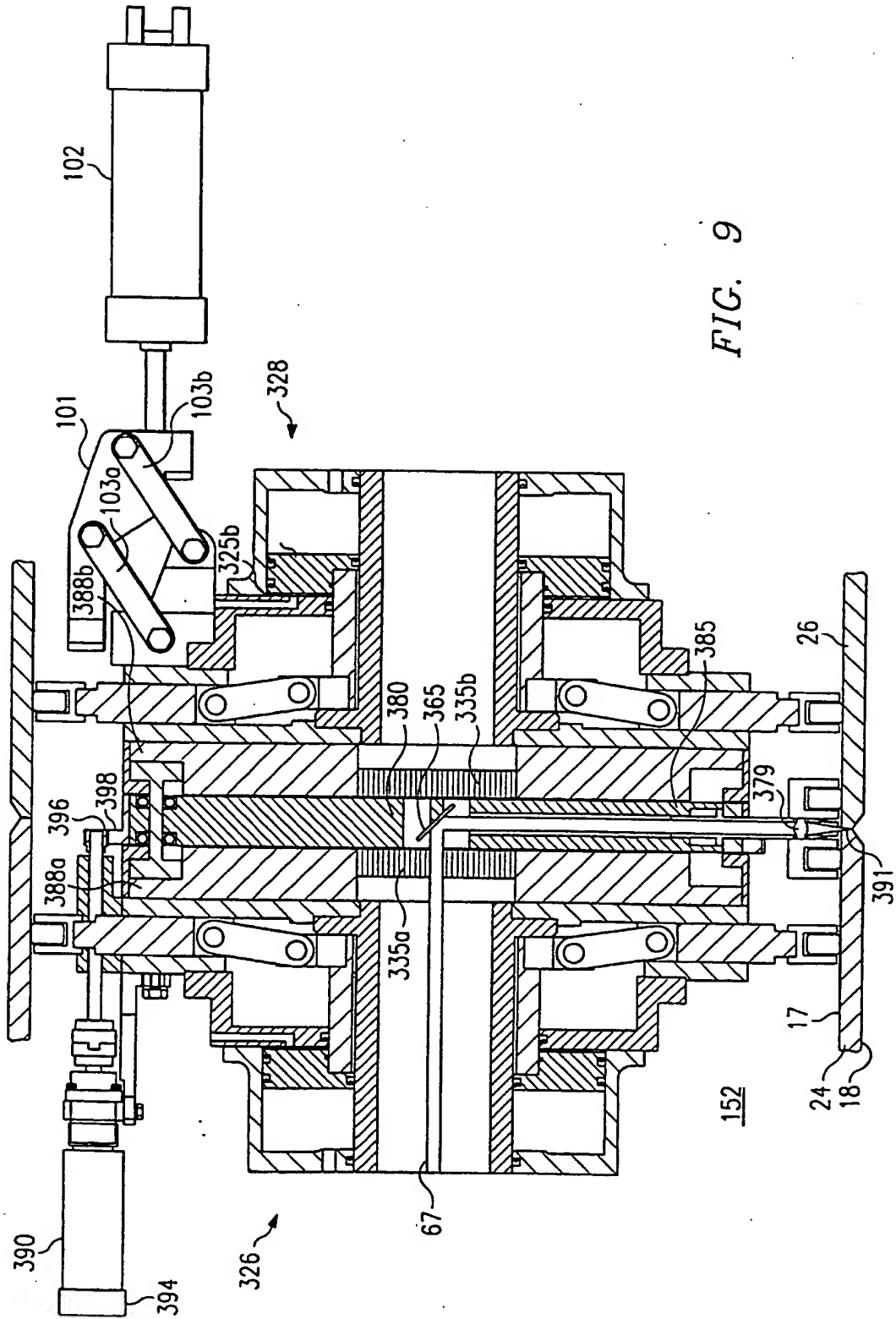


FIG. 9

FIG. 10

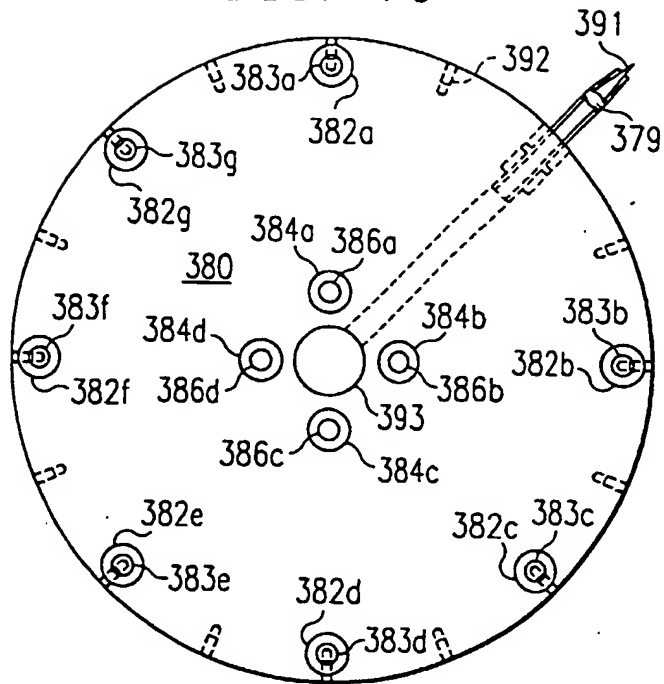


FIG. 11

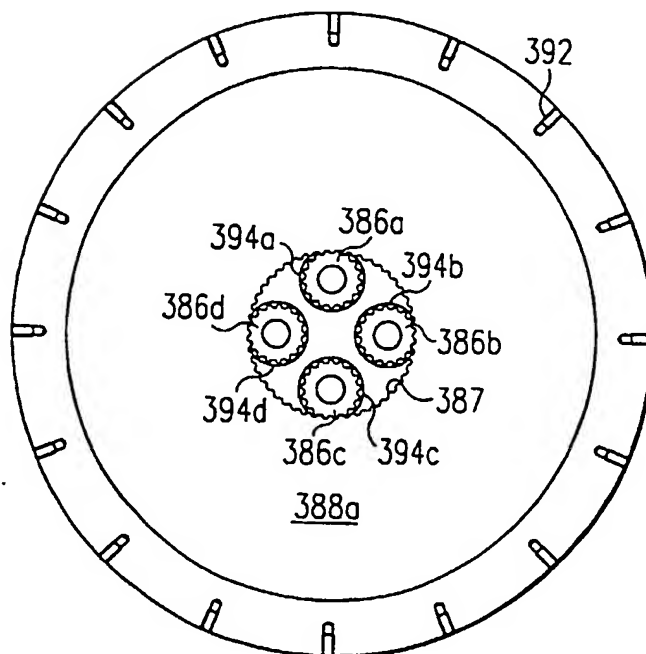
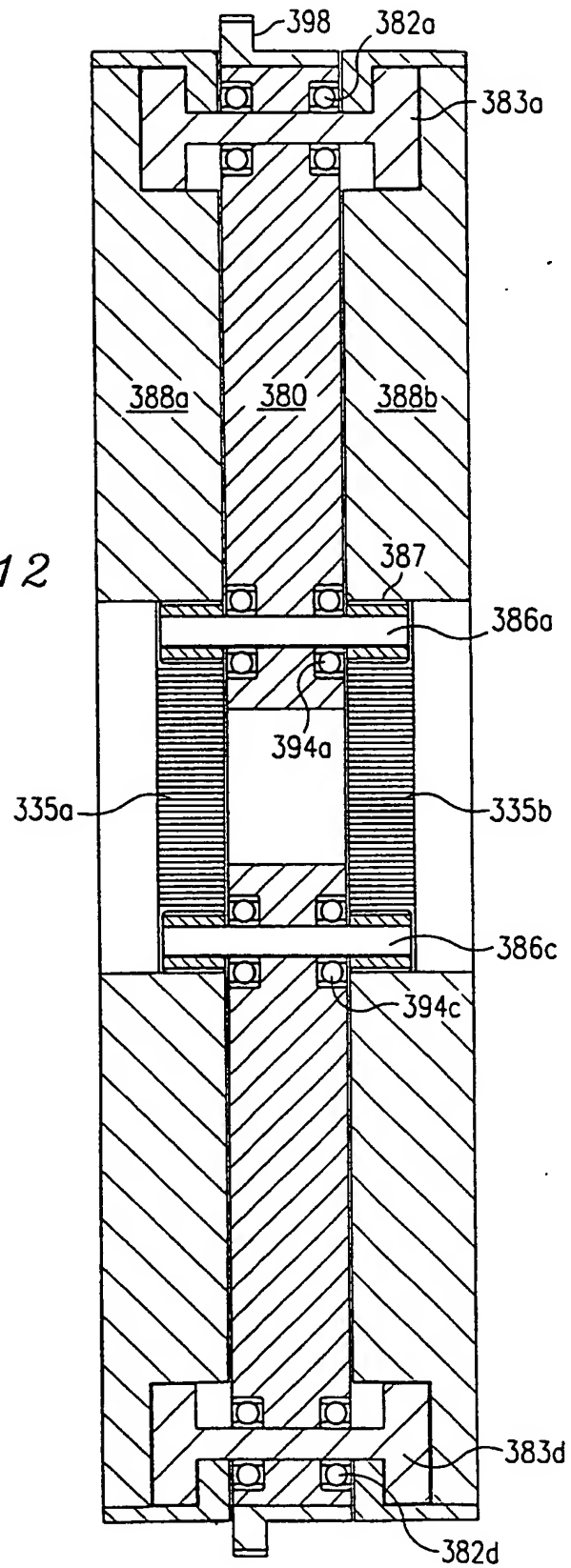
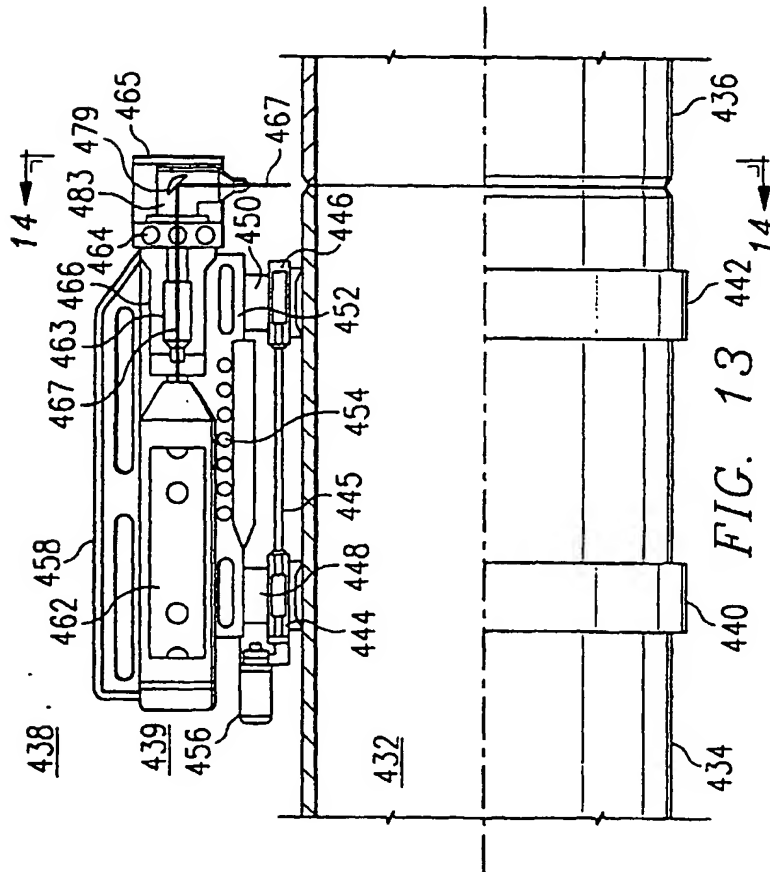
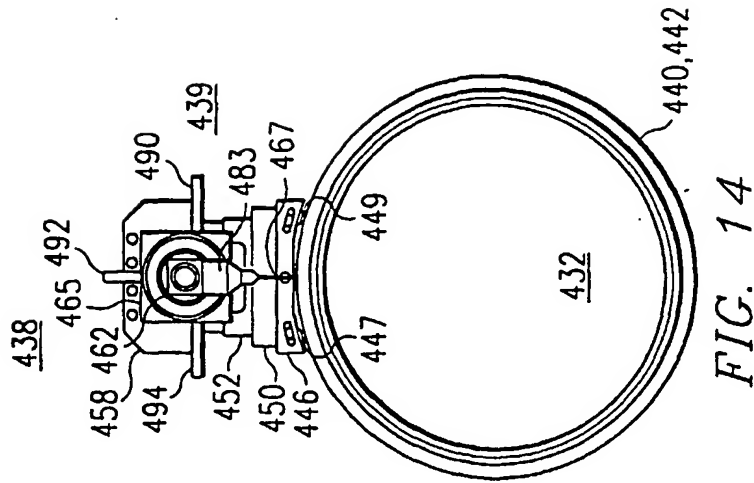


FIG. 12





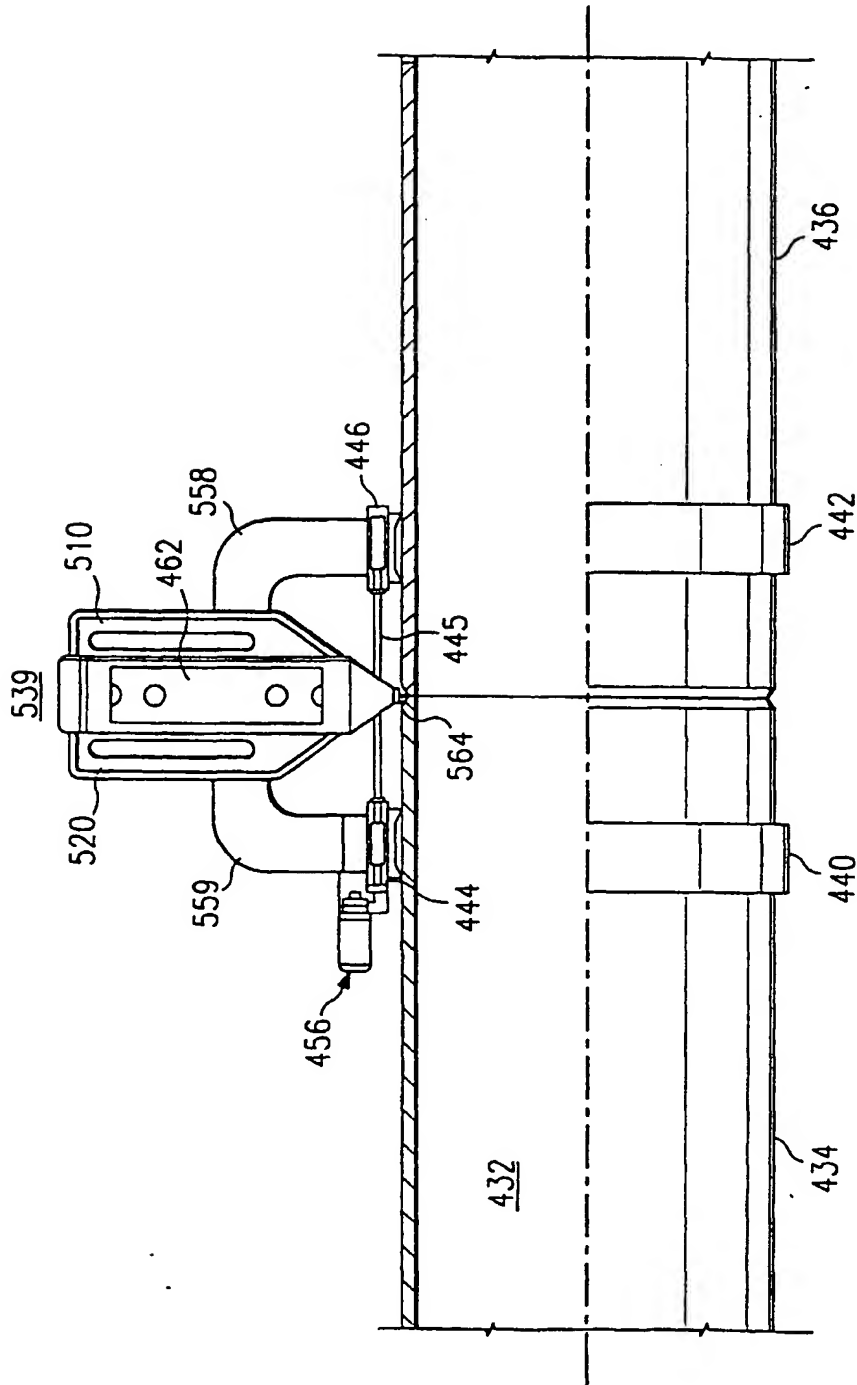


FIG. 15

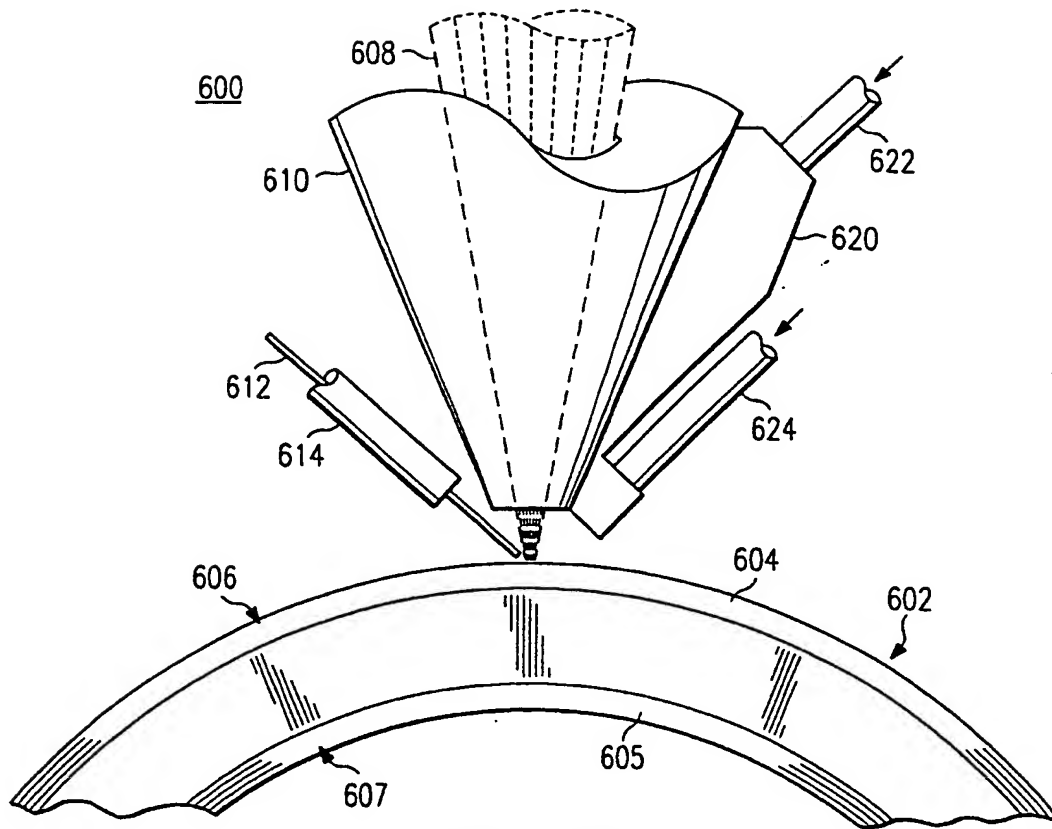


FIG. 16

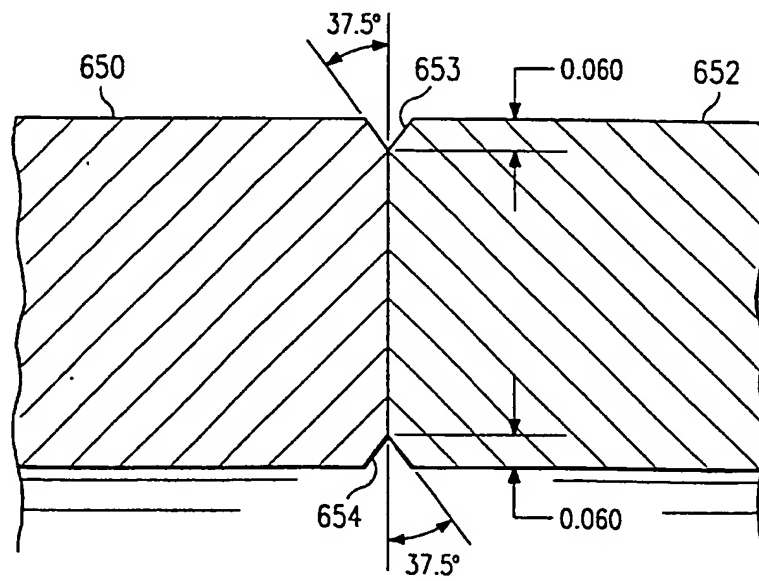


FIG. 17

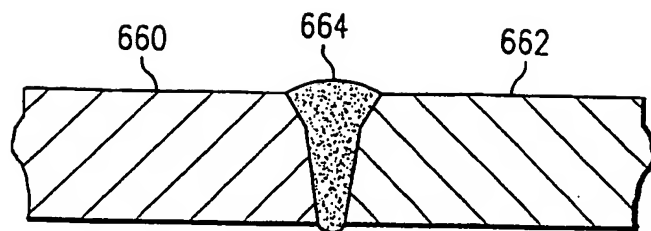


FIG. 18

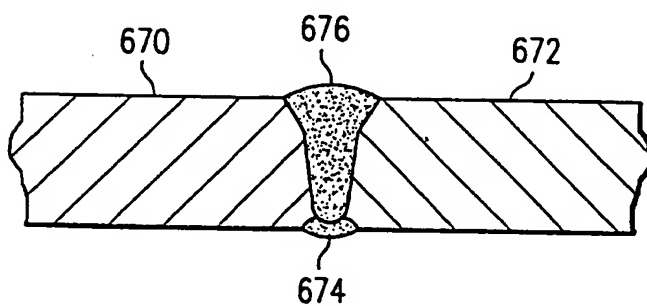


FIG. 19

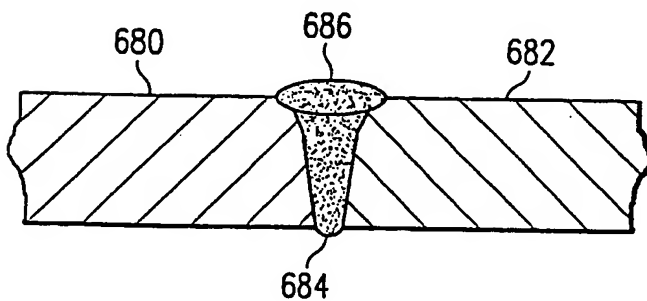


FIG. 20

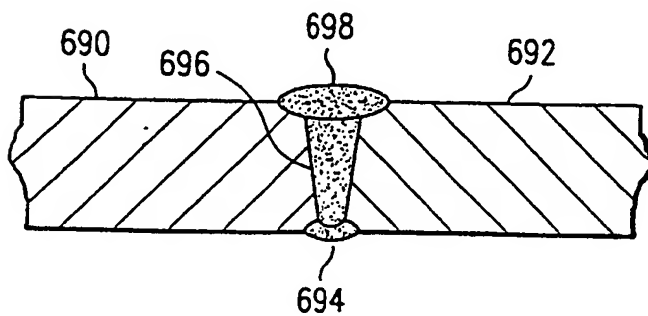


FIG. 21



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 97 25 0360

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X,D	US 4 001 543 A (BOVE OTTAVIO ET AL)	1-5	B23K9/028
Y	* column 10, line 10 - line 40; figures 2,3,7-12 *	8,9	B23K26/00
A	---	6,7	
X	US 4 213 025 A (KUHNEN GOTTFRIED)	6,7	
Y	* column 3, line 15 - line 28 *	8,9	
A	-----	1,2	
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			B23K
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
THE HAGUE		14 Apr11 1998	Aran, D
CATEGORY OF CITED DOCUMENTS			
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